# **Austempered Ductile Iron (ADI)**

## Alternative material for high performance applications

G. Artola<sup>1,4</sup>, I. Gallastegi<sup>1</sup>, J. Izaga<sup>1</sup>, M. Barreña<sup>2</sup> and A. Rimmer<sup>3</sup>

<sup>1</sup> IK4-Azterlan, Aliendalde Auzunea 6, 48200 Durango (Bizkaia), Spain

<sup>2</sup> Adilan Group, Pol. Ind. Santa Apolonia 2-2, 48215 Iurreta (Bizkaia), Spain

<sup>3</sup> ADI Treatments Ltd., Doranda Way, West Bromwich B71, UK

<sup>4</sup> Tecnun (University of Navarra), Paseo Manuel Lardizabal 13, 20018 Donostia (Gipuzkoa), Spain

ADI grades are standardized and the requirements of current international standards (EN 1564-12 / ASTM A897-15) are given in terms of conventional mechanical properties.

Nevertheless, these properties don't show the real potential of the ADI grades. In order to promote the use of ADI parts in place of other materials, this work proposes a comparison between ADI 900 and ADI 1200 grades, both in terms of conventional and advanced mechanical properties, employing stress intensity factors and critical CTODs (Crack Tip Opening Displacement).

This study is completed with mechanical fatigue testing, so that it can be shown that the service life of ADI parts is comparable to that given by other heavier and more expensive options.

*Keywords:* Austempered Ductile Iron, ADI, fracture mechanics, fatigue, alternative materials.

## 1. Introduction

Conventional mechanical testing is adequate for structural integrity calculations with ductile materials under plane stress conditions. When designs involve high strength materials, plane strains are more likely to occur and both fracture mechanics and fatigue become more relevant. This is the case for ADI and in this paper the characterization of two representative grades has been investigated.

## 2. Experimental method

All the materials in the tests planned have been processed in industrial facilities and under production conditions. It has been checked if the "as cast" materials are capable of reaching GJS-900-8 and GJS-1200-3 grades and, after austempering, a broad mechanical characterization has been performed.

All tests have followed European EN standards, except for fracture testing (BS) and uniaxial fatigue (ASTM).

## 3. Results and discussion

#### 3.1 "As cast" condition

The study materials have been obtained from 22 one-inch thickness type Y2 keel-blocks from the same heat. The "as cast" condition fulfils the requirements for a proper austempering treatment.

Table 1 Chemical composition (%)

			1	( )		
С	Si	Mn	Mg	Ni	Mo	Cu
3.69	2.28	0.19	0.037	2.45	0.20	0.79

rubie 2. meenanear properties as east i								
Hardness (HB10/3000W)	273							
Tongilo tosting	R <sub>p0.2</sub> (MPa)			R <sub>m</sub> (MPa)			A(%)	
Tensne testing	625			852 4.7			4.7	
Impost testing	KV (J)				Un	ed (J)		
impact testing	5	5	5	5	39	34	37	

Table 2. Mechanical properties "as cast"

Table 3 Microstructure.

Nodularity	Graphite density (nod./mm <sup>2</sup> )	Ferrite/pearlite ratio
>90	200	20/80

## 3.2 Austempering

The samples are machined to obtain two sets of specimen pre-shapes, with a minimum machining clearance of 2 mm. Austempering is performed under controlled atmosphere with a carbon potential of 0.8 during austenitization and inert gas protection during the transfer to the isothermal bath. After heat treatment, pre-shapes are machined to standard testing specimens and it is verified that one set of specimens has been obtained for each grade GJS-900-8 and GJS-1200-3.



Fig. 1 GJS-900-8 microstructure.



Fig. 2 GJS-1200-3 microstructure.

Table 5 GJS-900-8 m	echanical prop	erties.
---------------------	----------------	---------

Hardness (HB10/3000W)	314							
Tonsilo tosting	R <sub>p0.2</sub> (MPa)			R <sub>m</sub> (MPa)			A(%)	
Tensne testing	622			963 1			10.4	
Impost testing	KV (J)			Unnotch			ned (J)	
impact testing	8	9	9		105	99	106	

Table 6 GJS-1200-3 mechanical properties.

Hardness (HB10/3000W)	397							
Tongila tasting	$R_{p0.2}$ (MPa)			F	R <sub>m</sub> (MPa)			A (%)
Tensne testing	1035			1260				9.8
Impost testing	KV (J)		)	Unnotch		notch	lec	1 (J)
impact testing	7	7	8		104	102	2	94

BS7448-1 B(E) specimens with a 12.5x25 mm section have been employed for toughness testing. All fractures have shown an elastic-plastic behavior, despite the plasticity being small.

Table 7 Toughness testing.

U	U	
Grade	$K_Q (MPa \cdot m^{1/2})$	$\delta_{c}$ (mm)
GJS-900-8	50.3	0.05
GJS-1200-3	63.7	0.05

Fatigue curves have been built for an average stress  $\sigma_m$  equal to half  $R_{p0.2}$  of the grade tested. Loading amplitude  $\Delta\sigma$  ranged from 50% to  $100\% \cdot R_{p0.2}$ .



Fig. 3 S-N fatigue curves.

#### 4. Conclusions

GJS-900-8 and GJS-1200-3 grades develop plastic crack tip blunting for the studied thickness.

The obtained fatigue curves point to service lives that are higher than the reference values given in the European Standard.

The range of applications where ADI grades become an alternative material to current solutions is extended when design calculations take into account fracture and fatigue criteria.

#### Acknowledgements

The authors most sincerely thank to Furesa S.Coop., member of ADILAN Group, and to ADI Treatments Ltd. for their invaluable support in this work.

#### References

[1] A.Iglesias, I.Gallastegi, G.Artola, M.Muro et al.: 71st World Foundry Congress (2014).

[2] S.K. Putatunda: *Materials Science and Engineering* A315 (2001) 70-80.

[3] M.G. Hafiz: AFS Transactions (2009).

[4] M.Kuna, M.Springman, M.Mädler, P.Hübner and G.Pusch: *Engineering Fracture Mechanics* 72 (2005) 241-253.