

# An Analysis of Lamé Mode Resonators by Finite Difference Time Domain Method

ラーメモード振動子のFD-TD解析

Takashi Yasui<sup>1†</sup>, Koji Hasegawa<sup>2</sup>, and Koichi Hirayama<sup>1</sup> (<sup>1</sup>Kitami Institute of Tech.;  
<sup>2</sup>Grad. School of Eng., Muroran Institute of Tech.)  
安井 崇<sup>1†</sup>, 長谷川 弘治<sup>2</sup>, 平山 浩一<sup>1</sup> (<sup>1</sup>北見工大, <sup>2</sup>室蘭工大大学院)

## 1. Introduction

A staggered grid with the collocated grid points of velocities (SGCV) was presented for modeling propagation of elastic waves in anisotropic solids by finite-difference time-domain (FD-TD) method<sup>1</sup>. To impose boundary conditions on the FD-TD model simply, the new grid was derived from a single control volume of the momentum conservation law and line integrations of the displacement gradient. Abandoning the cross-shape arrangement of the velocity vector results in interpolations of the velocity components away from grid points. Numerical dispersions of vertically polarized shear waves (SV-waves) and longitudinal waves (P-waves) in an infinite isotropic solid by (2,2) and (2,4) schemes have been investigated and it has been reported<sup>1</sup> that the interpolation with 3rd degree bi-polynomials gives comparable results of conventional staggered grids<sup>2,3</sup>.

For modeling elastic wave devices by FD-TD method, boundary conditions on planar free surfaces should be examined. With the conventional staggered grids<sup>2,3</sup>, FD-TD models can use the stress-imaging technique<sup>3</sup>, the vacuum formalism<sup>4</sup> or the adjusted staggered scheme<sup>5</sup>. Because the velocity vectors are on the center grid points and all stresses on the grid surfaces are normal components in the FD-TD models with the SGCV, imposing of planar free surface conditions is to set all stress components on the surface zero. However, the interpolations of the velocity vectors away from the grid points near the free surface are required to compute velocity gradients. Hence a modification must be introduced. Extrapolation techniques or one-sided finite differentiation schemes are candidates for immediate computation of the velocity gradients on the grid points of stresses.

In this paper, for computation of velocity gradients, we will examine the derivatives of interpolation polynomials of velocity vector fields for the FD-TD models with the SGCV in two dimensions. We will extract the resonance frequency of the fundamental Lamé mode of a resonator on an isotropic solid and confirm the

validity of the SGCV models of the free surfaces.

## 2. Modeling Planar Free Surfaces by FD-TD with the SGCV in Two Dimensions

### 2.1 Time update equations by FD-TD scheme

In an isotropic solid in two dimensions, the cell of a uniform SGCV for SV- and P-waves propagation reduces to a grid shown in Fig. 1. Here,  $\Delta$  is the spatial interval of the grid,  $I$  and  $J$  are integers for a grid point with the position vector  $\mathbf{p} = (I\hat{x} + J\hat{y})\Delta$  where  $\hat{x}$ ,  $\hat{y}$  are the unit vector in the direction of  $x$ - and  $y$ -axis, and  $v_i$  and  $T_{ij}$  ( $i, j = x, y$ ) are the  $i$ -component of a particle velocity and the  $ij$ -component of a stress tensor.

Newton's equation of motion and relations of displacement gradient tensors  $\Gamma_{ij}$  and velocity vectors are modeled by FD-TD schemes in two dimensions as follows:

$$\rho D_{\mathbf{p},t}^T [v_i] = D_{\mathbf{p},x}^T [T_{ix}] + D_{\mathbf{p},y}^T [T_{iy}] \quad \text{for } i = x, y, \quad (1)$$

$$\partial \Gamma_{ij} / \partial t \Big|_{\mathbf{p}}^{T+\Delta t/2} = D_{\mathbf{p},j}^{T+\Delta t/2} [v_i] \quad \text{for } i, j = x, y. \quad (2)$$

Here,  $\rho$  is the mass density,  $t$  is time, and  $D_{\mathbf{p},i}^T [f]$  is a finite difference approximation of the spatial ( $i=x, y$ ) or time ( $i=t$ ) derivative of a scalar function  $f(\mathbf{r}, t)$  with respect to  $i$  on the grid point  $\mathbf{p}$  (●:eq. (1), □ and ○:eq. (2)) where  $T = K\Delta t$  with an integer  $K$  and the time interval  $\Delta t$ . Using the derivative of the stress and strain relation with respect to time and eq.(2), we obtain following relations:

$$D_{\mathbf{p},t}^{T+\Delta t/2} [T_{ij}] = \sum_{k,l} C_{ijkl} D_{\mathbf{p},l}^{T+\Delta t/2} [v_k] \quad \text{for } i, j = x, y. \quad (3)$$

The stiffness component  $C_{ijkl}$  of the isotropic solid is

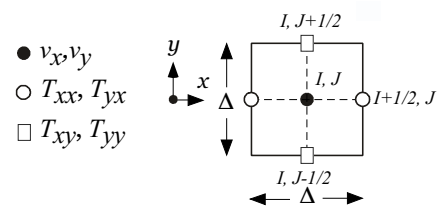


Fig.1 A unit cell of staggered grid with collocated grid points of velocities in two dimensions for SV- and P-waves propagation.

<sup>†</sup> yasui@mail.kitami-it.ac.jp

given by  $C_{ijkl} = \lambda\delta_{ij}\delta_{kl} + \mu(\delta_{ik}\delta_{jl} + \delta_{il}\delta_{jk})$ . Here  $\lambda$  and  $\mu$  are the Lamé constants, and  $\delta_{ij}$  is the Kronecker delta.

Velocity gradients  $D_{p,y}^{T+\Delta t/2}[v_k]$  and  $D_{p,x}^{T+\Delta t/2}[v_k]$  for  $k=x,y$  on the grid points of the stress components  $T_{kx}$  and  $T_{ky}$ , respectively, are required for the time update eq. (3). Using the finite difference approximation, therefore, velocity vectors on the four corners of the SGCV grid were interpolated in the elastic solid<sup>1)</sup>.

## 2.2 FD-TD model of free surfaces by SGCV

Consider an edge of a SGCV grid on a free surface. Velocity gradients  $D_{p,y}^{T+\Delta t/2}[v_k]$  or  $D_{p,x}^{T+\Delta t/2}[v_k]$  ( $k = x, y$ ) on the center point of the edge whose normal unit vector is  $\hat{x}$  or  $\hat{y}$ , respectively, cannot be computed by the interpolation scheme in the infinite solid<sup>1)</sup> because of lack of the grid points of the velocity vector in the vacuum. Recalling that the derivative of an interpolation polynomial is a scheme for numerical differentiation, we can compute the required gradients  $v_{k,x}$  or  $v_{k,y}$  on the edge immediately: when a tensor product of two polynomial interpolations of  $k$ -component of the velocity vector on adjoining grids,  $v_k(x, y) = \sum_{l=0}^{D_x-1} \sum_{m=0}^{D_y-1} C_{lm}(x-x_0)^l(y-y_0)^m$  for  $k=x, y$ , is used, we obtain  $v_{k,x}(x_0, y_0) = C_{10}$  or  $v_{k,y}(x_0, y_0) = C_{01}$ . Here, the coefficient  $C_{10}$  or  $C_{01}$  is computed by the  $(D_x \times D_y)$  values on the  $D_x$  and  $D_y$  adjoining grids in the  $x$ - and  $y$ -directions, respectively.

## 3. Analysis of a Lamé Mode Resonator

### 3.1 FD-TD models

In two dimensions, we consider a Lamé mode resonator that is a square with a side length of  $L$  on an isotropic solid with Poisson's ratio 0.25. When the wavelength of the SV-wave at the frequency  $f_s$  is  $2L$ , the fundamental resonance frequency  $f_1$  of the Lamé mode is  $f_1 = \sqrt{2}f_s$ . In the following results,  $f_1 = 1\text{MHz}$  and  $R = \frac{v_p\Delta t}{\Delta} = 0.5$ , where  $v_p$  is the phase velocity of the P-wave in the infinite solid. Near the free surface, for computation of  $v_{k,x}(x_0, y_0)$  or  $v_{k,y}(x_0, y_0)$ , we choose  $D_x = D_y = 2$  or  $D_j = 3$  and the other of 2. In the solid away from the surfaces, we use a bilinear polynomial interpolation with four nodes for computation of  $D_{p,y}^{T+\Delta t/2}[v_k]$  and  $D_{p,x}^{T+\Delta t/2}[v_k]$ .

### 3.2 Computation of the resonance frequency

The observation point and vibration point are  $(L/4, L/4)$  and  $(-L/4, -L/4)$  on the  $x$ - $y$  plane with

the origin on the center of the square resonator. The vibration of the  $x$ -component of the particle velocity expressed as a sine-modulated Gaussian pulse with the center frequency  $f_1$  and the half-width in time  $83.26RL/v_p$  yields a discrete time response of the particle velocity of the observation point as shown in **Fig. 2**. Applying the discrete Fourier transform to the time response at the observation point in an interval from  $N_s\Delta t$  to  $N_e\Delta t$ , we extract the resonance frequency of the resonator. **Figure 3** shows the power spectrum with  $L/h = 2^6$ ,  $N_s\Delta t = 2^8 RL/v_p \approx 52.26\mu\text{s}$ ,  $N_e\Delta t = 2^{16} RL/v_p$  and the coefficients,  $C_{10}$  or  $C_{01}$ , computed by the six adjoining grids. Extracted resonance frequency is 0.9999MHz and we may confirm the validity of our free surface models.

**Figure 4** shows extracted resonance frequencies with  $N_s\Delta t = 2^8 RL/v_p \approx 52.26\mu\text{s}$  and  $N_e\Delta t = 2^N RL/v_p$ . Computed results by four and six adjoining grids with  $L/h = 4$  are 0.992 and 0.985MHz, respectively, and we expect that use of six adjoining grids is preferable for an accurate model.

## References

1. K. Hasegawa and T. Shimada: Jpn. J. Appl. Phys. **51** (2012) 07GB04.
2. J. Virieux: Geophysics **51** (1986) 889.
3. A. Levander: Geophysics **53** (1988) 1425.
4. J. Zahradnil and E. Priolo: Geophys. J. Int. **120** (1995) 663.
5. J. Kristek, P. Moczo and R.J. Archuleta: Studia Geophys. Geodet. **46** (2002) 355.

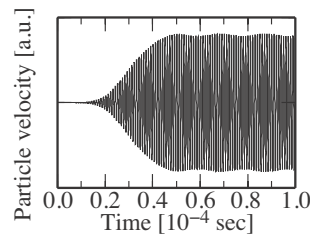


Fig.2 A time response at the observation point.

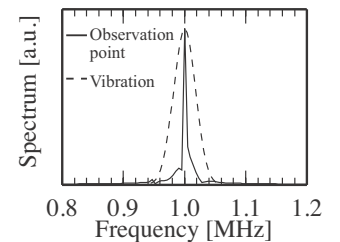


Fig.3 Power spectra of  $x$ -components of particle velocities of the vibration and observation points.

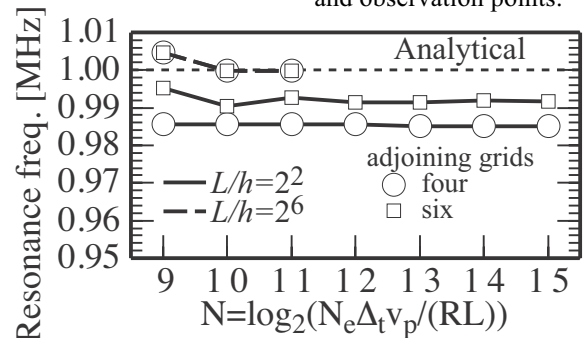


Fig.4 Extracted resonance frequencies.